



Civil & Structural Engineering Design Services Pty. Ltd.

Client: Hercules Instant Shelter Australia Pty Ltd

Project: Design check –3m × 3m, 3m × 4.5m & 3m × 6m HEX 45A Folding Marquee Structures for 50km/hr Wind Speed.

Reference: Hercules Instant Shelter Australia's Technical Data

Report by: KZ

Checked by: EAB

Date: 05/04/2021

JOB NO: D-11-268664-5



Civil & Structural Engineering Design Services Pty. Ltd.

Table of Contents

1	Introduction.....	3
2	Design Restrictions and Limitations	4
3	Specifications	5
3.1	General	5
3.2	Section Properties.....	6
4	Buckling Constant.....	6
5	Design Loads.....	7
5.1	Ultimate.....	7
5.2	Load Combinations	7
5.2.1	Serviceability.....	7
5.2.2	Ultimate	7
6	Wind Analysis.....	7
6.1	Parameters.....	7
6.2	Pressure Coefficients (C_{fig}).....	8
6.2.1	Pressure summary.....	8
6.3	Wind Load Diagrams	11
6.3.1	Wind 1(case 1).....	11
6.3.2	Wind 1(case 2).....	11
6.3.3	Wind 2(Case1).....	12
6.3.4	Wind 2(case 2).....	12
6.3.5	Max Bending Moment due to critical load combination in major axis.....	13
6.3.6	Max Bending Moment in minor axis due to critical load combination	13
6.3.7	Max Shear in due to critical load combination	14
6.3.8	Max Axial force in upright support and roof beam due to critical load combination	14
6.3.9	Max reactions	15
6.4	Summary Forces.....	15
7	Checking Members Based on 1664.1:1997 Aluminum Structures Limit State Design.....	16
7.1	Truss Bars.....	16
7.2	Legs.....	20
7.3	Centre Pole.....	24
8	Summary	29
8.1	Conclusions	29



Civil & Structural Engineering Design Services Pty. Ltd.

1 Introduction

This Certification is the sole property for copyright of Mr. Ted Bennett of Civil & Structural Engineering Design Services Pty. Ltd. and the license holder for the exclusive use of this Certification, Hercules Instant Shelter Australia Pty Ltd.

The following structural drawings and calculations are for the applicable transportable marquees supplied by Hercules Instant Shelter Australia Pty Ltd.

The report examines the effect of 3s gust wind of 50 km/hr on 3m x 6m HEX 45A Folding Marquee as the worst-case scenario. The relevant Australian Standards AS1170.0:2002 General principles, AS1170.1:2002 Permanent, imposed and other actions and AS1170.2:2011 Wind actions are used. The design check is in accordance with AS/NZS 1664.1:1997 Aluminum Structures Limit State Design.



2 Design Restrictions and Limitations

- 2.1 The erected structure is for temporary use only.
- 2.2 It should be noted that if high gust wind speeds are anticipated or forecast in the locality of the marquee, the temporary erected structure should be dismantled.
- 2.3 For forecast winds in excess of (**refer to summary**) the structure should be completely folded.
(Please note that the locality squall or gust wind speed is affected by factors such as terrain exposure and site elevations.)
- 2.4 The structure may only be erected in regions with wind classifications no greater than the limits specified on the attached wind analysis.
- 2.5 The wind classifications are based upon category 2 in AS/NZS1170.2. Considerations have also been made to the regional wind terrain category, topographical location and site shielding from adjacent structures. Please note that in many instances topographical factors such as a location on the crest of a hill or on top of an escarpment may yield a higher wind speed classification than that derived for a higher wind terrain category in a level topographical region. For this reason, particular regard shall be paid to the topographical location of the structure. For localities which do not conform to the standard prescribed descriptions for wind classes as defined above, a qualified Structural Engineer may be employed to determine an appropriate wind class for that the particular site.
- 2.6 The structures in no circumstances shall ever be erected in tropical or severe tropical cyclonic condition.
- 2.7 The marquee structure has not been designed to withstand snow and ice loadings such as when erected in alpine regions.
- 2.8 For the projects, where the site conditions approach the design limits, extra consideration should be given to pullout tests of the stakes and professional assessment of the appropriate wind classification for the site.
- 2.9 No Fabrics or doors should be used for covering the sides of unbraced Folding Marquees due to the lack of bracing within the system and insufficient out-of-plane stiffness of framing.

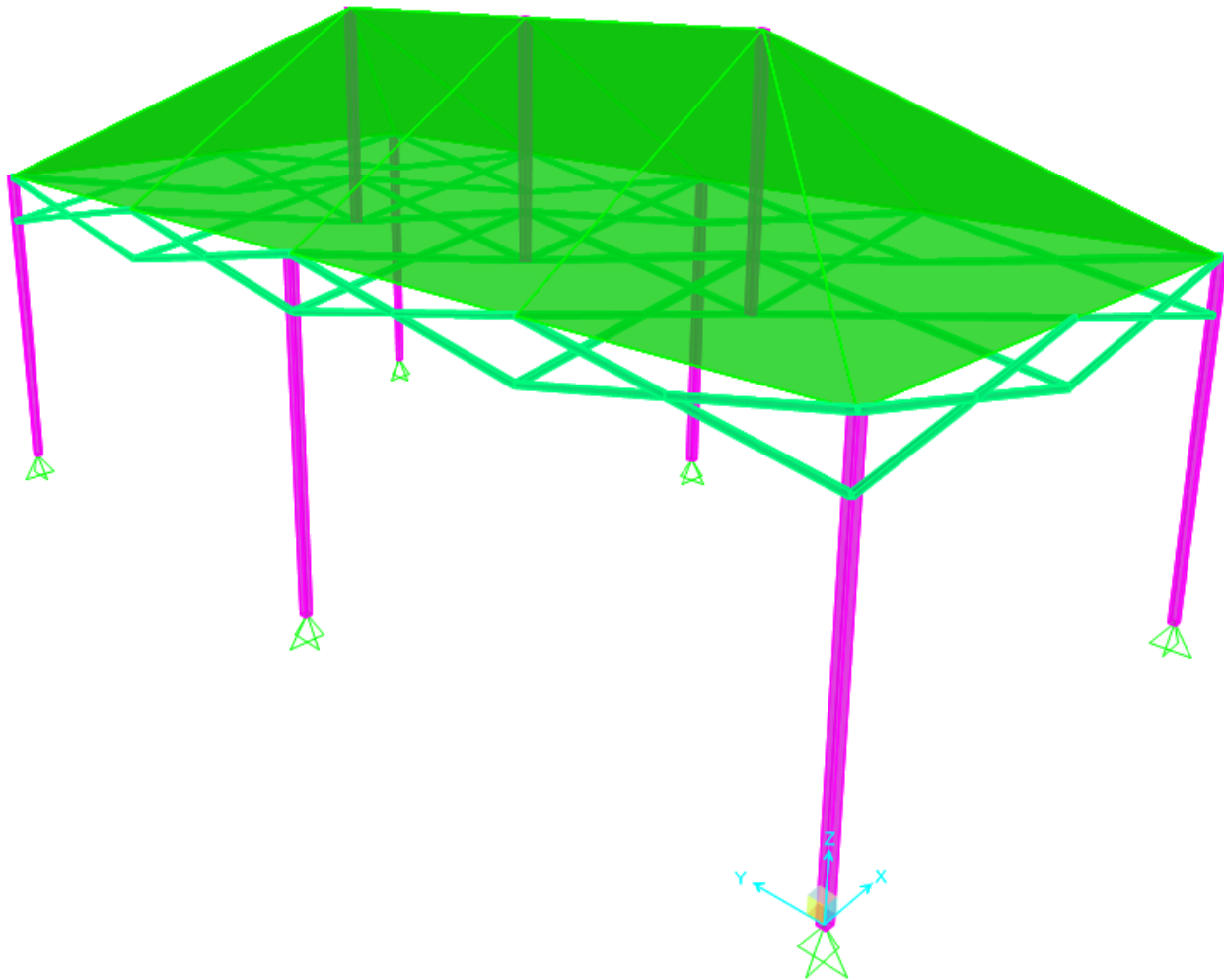


3 Specifications

3.1 General

Marquee category	
Material	Aluminum 6005-T5

Size	Model
3m x 6m	Folding Marquees – HEX 45A

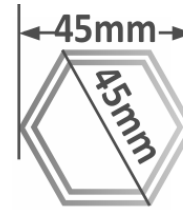




Civil & Structural Engineering Design Services Pty. Ltd.

3.2 Section Properties

-Legs: 40x40x2 SHS profile
 -Thickness: 2.0mm
 -Truss bars: 32x16x2.0



MEMBER(S)	Section	b	d	t	y _c	A _g	Z _x	Z _y	S _x	S _y	I _x	I _y	J	r _x	r _y
		mm	mm	mm	mm	mm ²	mm ³	mm ³	mm ³	mm ³	mm ⁴	mm ⁴	mm ⁴	mm	mm
Legs	HEX45	45	45	1.5	22.5	194.7	2458.0	2458.0	1690.0	1690.0	38030.0	38030.0	69246.0	14.0	14.0
Centre Pole	HEX45	45	45	1.5	22.5	194.7	2458.0	2458.0	1690.0	1690.0	38030.0	38030.0	69246.0	14.0	14.0
Truss Bar	25x12.5x1.5	12.5	25	1	12.5	71.0	450.4	296.0	564.5	342.6	5629.9	1850.2	4291.6	8.9	5.1

4 Buckling Constant

TABLE 3.3(D)
BUCKLING CONSTANTS FOR ALLOY 6005-T5

Type of member and stress	Intercept, MPa		Slope, MPa		Intersection	
Compression in columns and beam flanges	B_c	271.04	D_c	1.69	C_c	65.89
Compression in flat plates	B_p	310.11	D_p	2.06	C_p	61.60
Compression in round tubes under axial end load	B_t	297.39	D_t	10.70	C_t	*
Compressive bending stress in rectangular bars	B_{br}	459.89	D_{br}	4.57	C_{br}	67.16
Compressive bending stress in round tubes	B_{tb}	653.34	D_{tb}	50.95	C_{tb}	78.23
Shear stress in flat plates	B_s	178.29	D_s	0.90	C_s	81.24
Ultimate strength of flat plates in compression	<i>k</i> ₁	0.35	<i>k</i> ₂	2.27		
Ultimate strength of flat plates in bending	<i>k</i> ₁	0.5	<i>k</i> ₂	2.04		

* *C_t* shall be determined using a plot of curves of limit state stress based on elastic and inelastic buckling or by trial and error solution



Civil & Structural Engineering Design Services Pty. Ltd.

5 Design Loads

5.1 Ultimate

		Distributed load (kPa)	Design load factor (-)	Factored imposed load (kPa)
Live	Q	-	1.5	-
Self weight	G	self weight	1.35, 1.2, 0.9	1.2 self weight, 0.9 self weight
3s 50km/hr gust	W	0.096 C _{fig}	1.0	0.096 C _{fig}

5.2 Load Combinations

5.2.1 Serviceability

$$\text{Gravity} = 1.0 \times G$$

$$\text{Wind} = 1.0 \times G + 1.0 \times W$$

5.2.2 Ultimate

$$\begin{aligned} \text{Downward} &= 1.35 \times G \\ &= 1.2 \times G + W_u \end{aligned}$$

$$\text{Upward} = 0.9 \times G + W_u$$

6 Wind Analysis

Wind towards surface (+ve), away from surface (-ve)

6.1 Parameters

Terrain category = 2

Site wind speed ($V_{\text{sit},\beta}$) = $V_R M_d (M_{z,\text{cat}} M_s M_t)$

$V_R = 13.89 \text{ m/s (50 km/hr)}$

(regional 3 s gust wind speed)

$M_d = 1$

$M_s = 1$

$M_t = 1$

$M_{z,\text{cat}} = 0.91$

(Table 4.1(B) AS1170.2)

$V_{\text{sit},\beta} = 12.64 \text{ m/s}$

Height of structure (h) = 2.83 m

(mid of peak and eave)

Width of structure (w) = 3 m

Length of structure (l) = 6 m

Pressure (P) = $0.5 \rho_{\text{air}} (V_{\text{sit},\beta})^2 C_{\text{fig}} C_{\text{dyn}}$
 = 0.096 C_{fig} kPa



Civil & Structural Engineering Design Services Pty. Ltd.

6.2 Pressure Coefficients (C_{fig})

Name	Symbol	Value	Unit	Notes	Ref.
Input					
Importance level		2			Table 3.1 - Table 3.2 (AS1170.0)
Annual probability of exceedance		Temporary			Table 3.3
Regional gust wind speed		50	Km/hr		Table 3.1 (AS1170.2)
Regional gust wind speed	V_R	13.89	m/s		
Wind Direction Multipliers	M_d	1			Table 3.2 (AS1170.2)
Terrain Category Multiplier	$M_{z,cat}$	0.91			Table 4.1 (AS1170.2)
Shield Multiplier	M_s	1			4.3 (AS1170.2)
Topographic Multiplier	M_t	1			4.4 (AS1170.2)
Site Wind Speed	$V_{Site,\beta}$	12.64	m/s	$V_{Site,\beta} = V_R * M_d * M_{z,cat} * M_s * M_t$	
Pitch	α	30	Deg		
Pitch	α	0.52	rad		
Width	B	3	m		
Length	D	6	m		
Height	Z	2.83	m		
Wind Pressure					
ρ_{air}	ρ	1.2	Kg/m ³		
dynamic response factor	C_{dyn}	1			
Wind Pressure	$\rho * C_{fig}$	0.096	Kg/m ²	$\rho = 0.5 \rho_{air} * (V_{des,\beta})^2 * C_{fig} * C_{dyn}$	2.4 (AS1170.2)
WIND DIRECTION 1 ($\theta=0,180$)					
4. Free Roof				$\alpha=0^\circ$	
Area Reduction Factor	K_a	1			D7
local pressure factor	K_l	1			
porous cladding reduction factor	K_p	1			
External Pressure Coefficient MIN	$C_{P,w}$	-0.3			



Civil & Structural Engineering Design Services Pty. Ltd.

External Pressure Coefficient MAX	$C_{P,w}$	0.8	
External Pressure Coefficient MIN	$C_{P,l}$	-0.7	
External Pressure Coefficient MAX	$C_{P,l}$	0	
aerodynamic shape factor MIN	$C_{fig,w}$	-0.30	
aerodynamic shape factor MAX	$C_{fig,w}$	0.80	
aerodynamic shape factor MIN	$C_{fig,l}$	-0.70	
aerodynamic shape factor MAX	$C_{fig,l}$	0.00	
Pressure Windward MIN	P	-0.03	kPa
Pressure Windward MAX	P	0.08	kPa
Pressure Leeward MIN	P	-0.07	kPa
Pressure Leeward MAX	P	0.00	kPa

WIND DIRECTION 2 ($\theta=90,270$)

4. Free Roof

Area Reduction Factor	K_a	1	
local pressure factor	K_l	1	
porous cladding reduction factor	K_p	1	
External Pressure Coefficient MIN	$C_{P,w}$	-0.3	
External Pressure Coefficient MAX	$C_{P,w}$	0.4	
External Pressure Coefficient MIN	$C_{P,l}$	-0.4	
External Pressure Coefficient MAX	$C_{P,l}$	0	
aerodynamic shape factor MIN	$C_{fig,w}$	-0.30	
aerodynamic shape factor MAX	$C_{fig,w}$	0.40	
aerodynamic shape factor MIN	$C_{fig,l}$	-0.40	
aerodynamic shape factor MAX	$C_{fig,l}$	0.00	
Pressure MIN (Windward Side)	P	-0.03	kPa
Pressure MAX (Windward Side)	P	0.04	kPa
Pressure MIN (Leeward Side)	P	-0.04	kPa
Pressure MAX (Leeward Side)	P	0.00	kPa

$\alpha=180^\circ$

D7



6.2.1 Pressure summary

WIND EXTERNAL PRESSURE	Direction1		Direction2		
	Min (Kpa)	Max (Kpa)		Min (Kpa)	Max (Kpa)
W	-0.03	0.08	W	-0.03	0.04
L	-0.07	0.00	L	-0.04	0.00

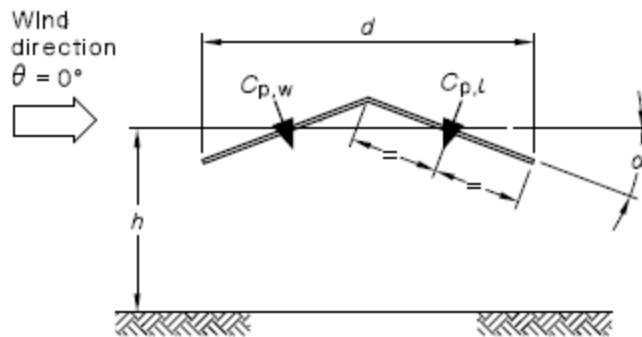
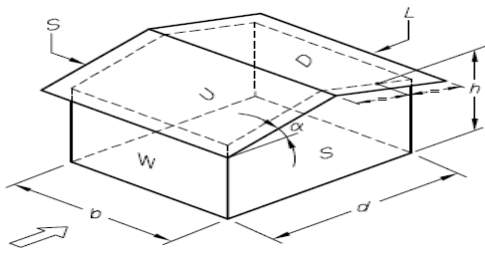
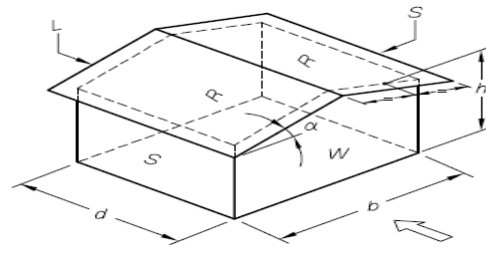


FIGURE D3 PITCHED FREE ROOFS



Direction 1



Direction 2

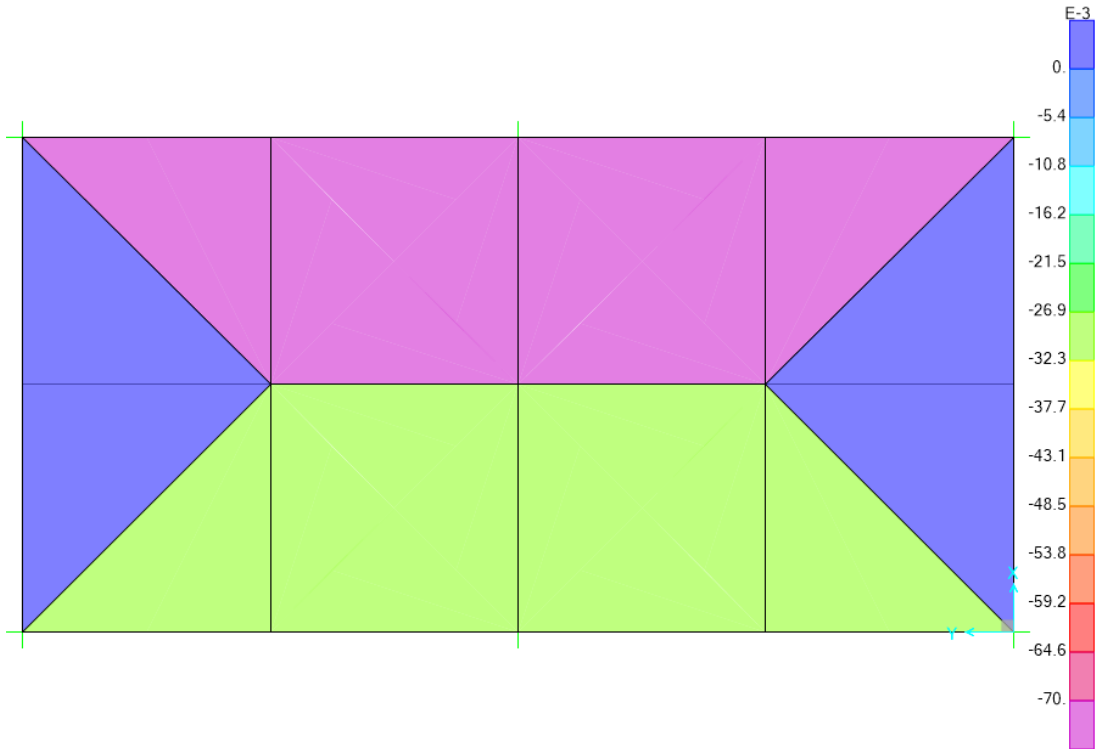
AS1170.2



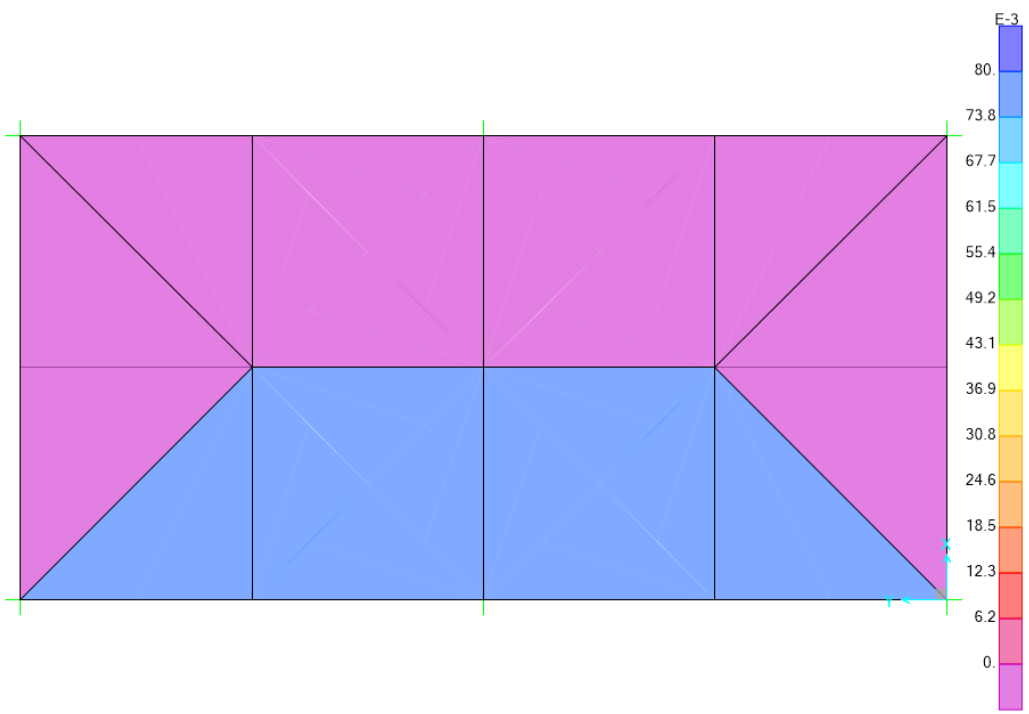
Civil & Structural Engineering Design Services Pty. Ltd.

6.3 Wind Load Diagrams

6.3.1 Wind 1(case 1)



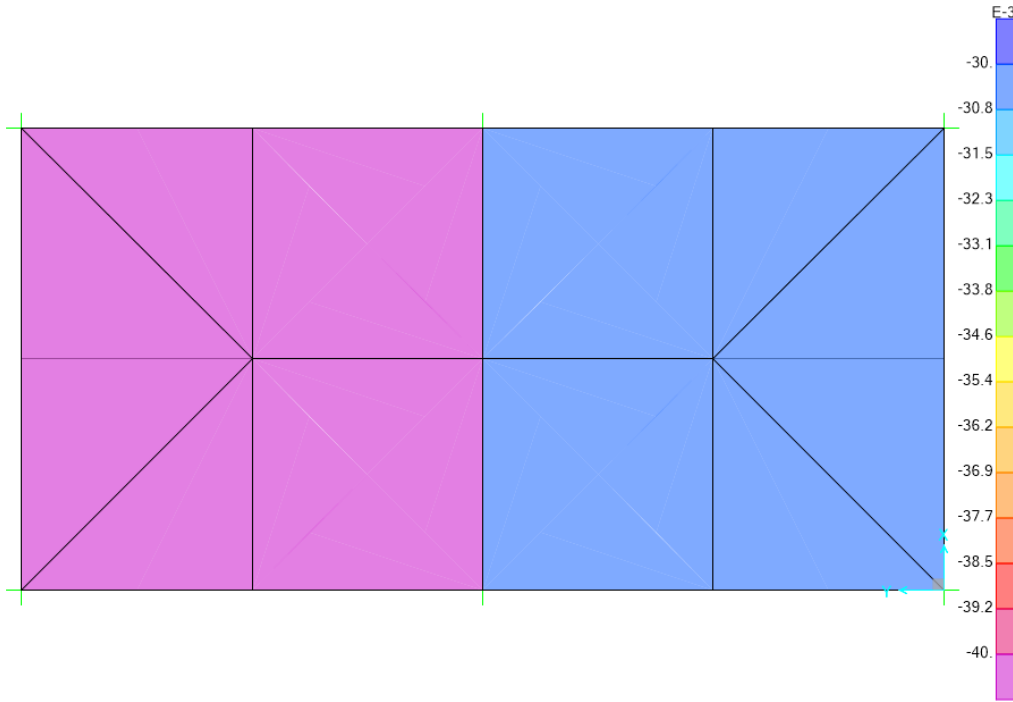
6.3.2 Wind 1(case 2)



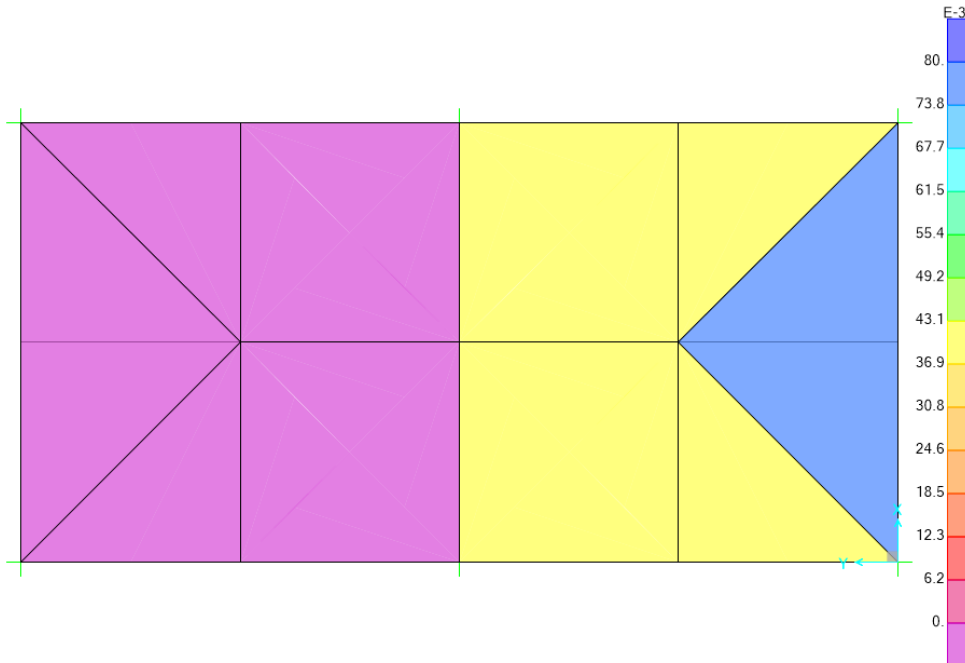


Civil & Structural Engineering Design Services Pty. Ltd.

6.3.3 Wind 2(Case1)



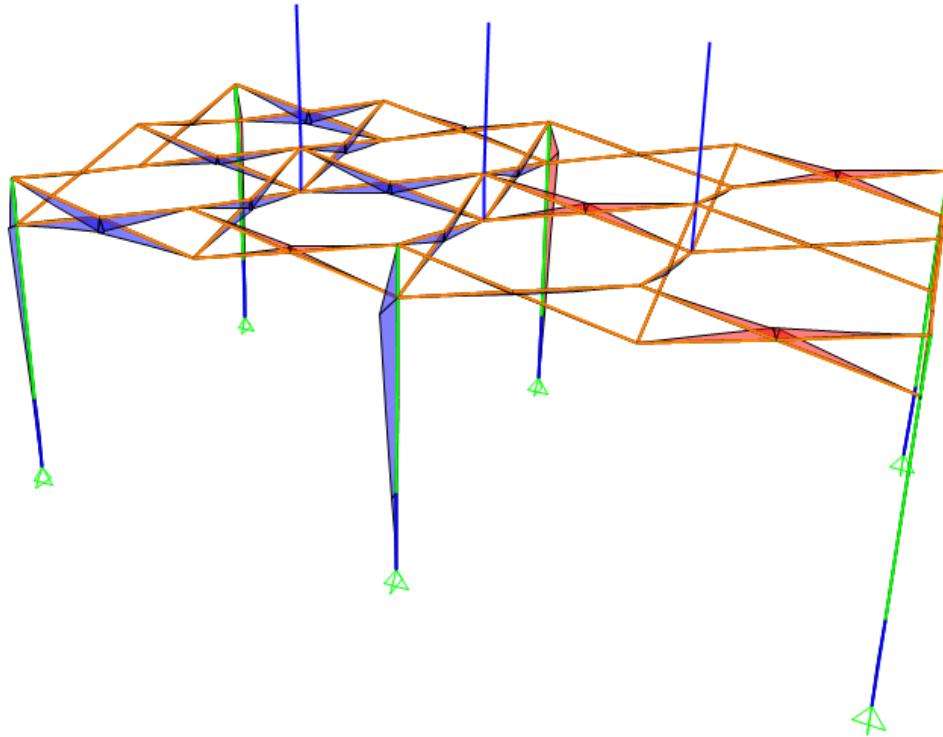
6.3.4 Wind 2(case 2)



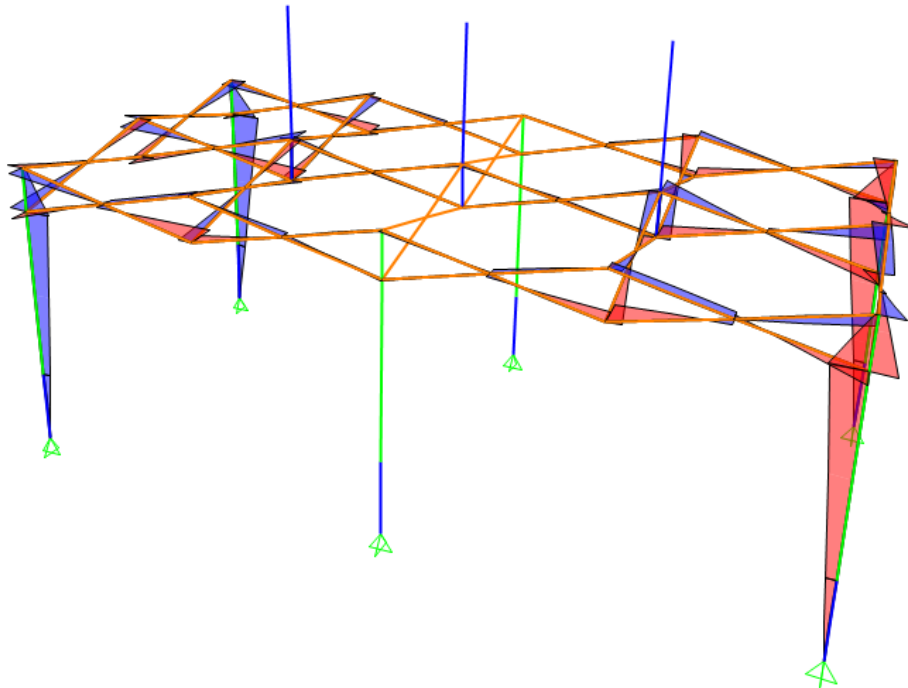
After 3D model analysis, each member is checked based on adverse load combination. In this regard the maximum bending moment, shear and axial force due to adverse load combinations for each member are presented as below:



6.3.5 Max Bending Moment due to critical load combination in major axis



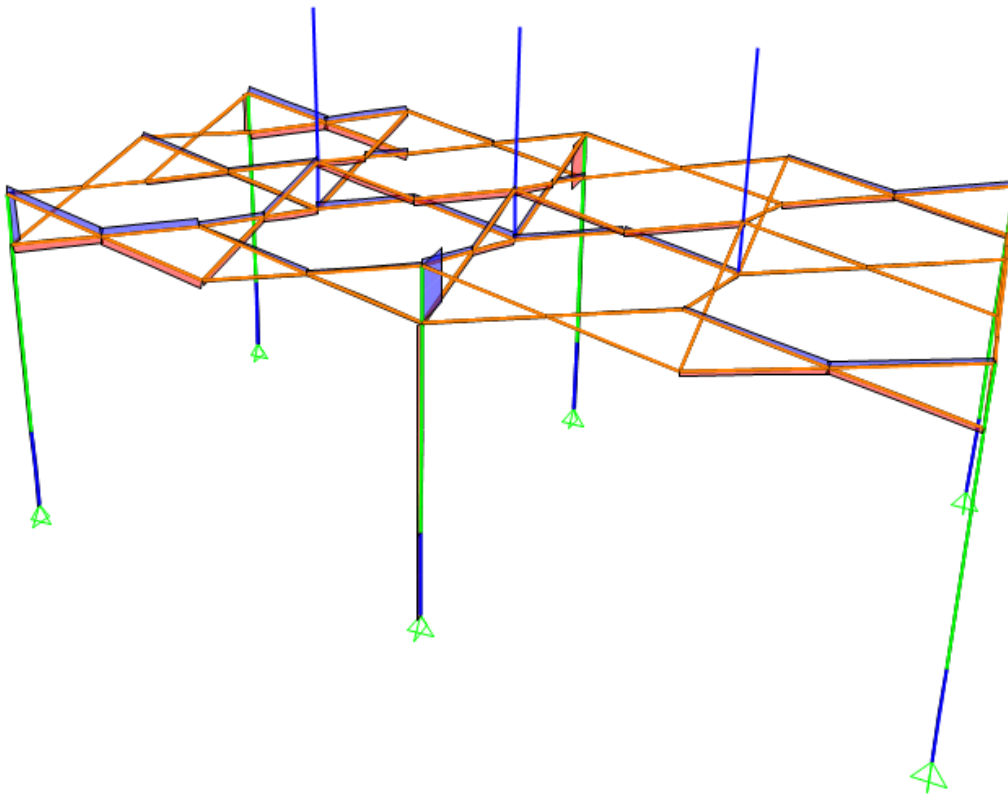
6.3.6 Max Bending Moment in minor axis due to critical load combination



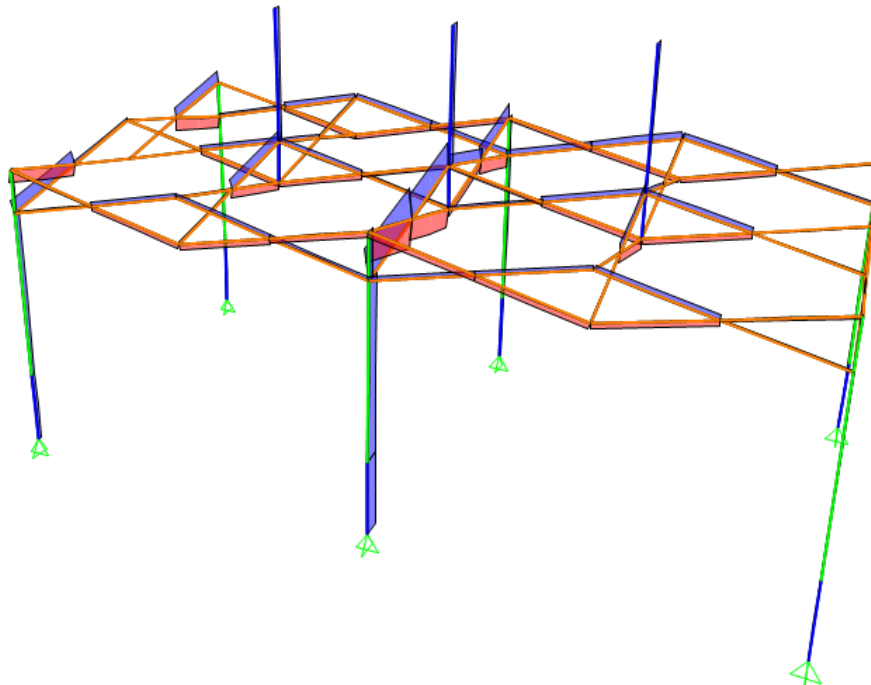


Civil & Structural Engineering Design Services Pty. Ltd.

6.3.7 Max Shear in due to critical load combination



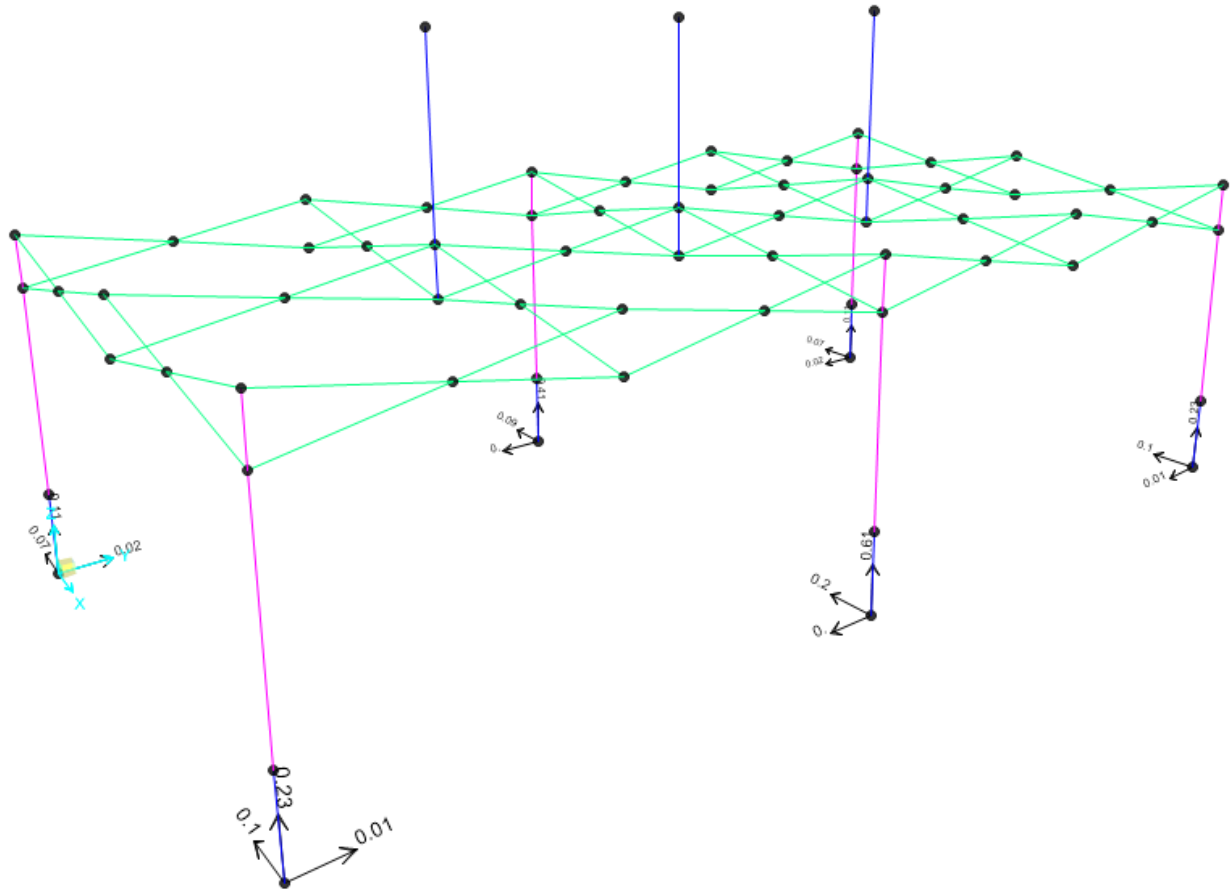
6.3.8 Max Axial force in upright support and roof beam due to critical load combination





Civil & Structural Engineering Design Services Pty. Ltd.

6.3.9 Max reactions



Max Uplift $N^* = 0.35\text{kN}$

6.4 Summary Forces

MEMBER(S)	Section	b	d	t	Vx	Vy	P (Axial)	Mx	My
		mm	mm	mm	kN	kN	kN	kN.m	kN.m
Legs	HEX45	45	45	1.5	0.096	-3E-14	-0.318	-0.1928	5.931E-14
Centre Pole	HEX45	45	45	1.5	0.055	-1.2E-17	-0.096	0.0508	-1.644E-16
Truss Bar	25x12.5x1.5	12.5	25	1	0.056	1.1E-14	-0.303	0.0443	7.207E-16



7 Checking Members Based on 1664.1:1997 Aluminum Structures Limit State Design

7.1 Truss Bars

NAME	SYMBOL	VALUE	UNIT	NOTES	REF
25x12.5x1.5	Truss Bar				
Alloy and temper	6005-T5				AS1664.1
Tension	F_{tu}	= 262	MPa	<i>Ultimate</i>	T3.3(A)
	F_{ty}	= 241	MPa	<i>Yield</i>	
Compression	F_{cy}	= 241	MPa		
Shear	F_{su}	= 165	MPa	<i>Ultimate</i>	
	F_{sy}	= 138	MPa	<i>Yield</i>	
Bearing	F_{bu}	= 138	MPa	<i>Ultimate</i>	
	F_{by}	= 386	MPa	<i>Yield</i>	
Modulus of elasticity	E	= 70000	MPa	<i>Compressive</i>	
	k_t	= 1			T3.4(B)
	k_c	= 1			
FEM ANALYSIS RESULTS					
Axial force	P	= 0.303	kN	<i>compression</i>	
	P	= 0	kN	<i>Tension</i>	
In plane moment	M_x	= 0.0443	kNm		
Out of plane moment	M_y	= 7.207E-16	kNm		
DESIGN STRESSES					
Gross cross section area	A_g	= 71	mm ²		
In-plane elastic section modulus	Z_x	= 450.39333	mm ³		
Out-of-plane elastic section mod.	Z_y	= 296.03667	mm ³		
Stress from axial force	f_a	= P/A_g			
		= 4.27	MPa	<i>compression</i>	
		= 0.00	MPa	<i>Tension</i>	
Stress from in-plane bending	f_{bx}	= M_x/Z_x			
		= 98.36	MPa	<i>compression</i>	



Civil & Structural Engineering Design Services Pty. Ltd.

Stress from out-of-plane bending	f_{by}	=	M_y/Z_y		
		=	0.00	MPa	<i>compression</i>
<i>Tension</i>					
3.4.3 Tension in rectangular tubes					
	ϕF_L	=	228.95	MPa	
		OR			
	ϕF_L	=	222.70	MPa	
COMPRESSION					
3.4.8 Compression in columns, axial, gross section					
<i>1. General</i>					
					... 3.4.8.1
Unsupported length of member	L	=	1544	mm	
Effective length factor	k	=	1.00		
Radius of gyration about buckling axis (Y)	r_y	=	5.10	mm	
Radius of gyration about buckling axis (X)	r_x	=	8.90	mm	
Slenderness ratio	kLb/r_y	=	151.23		
Slenderness ratio	kL/r_x	=	173.39		
Slenderness parameter	λ	=	3.24		
	D_c^*	=	90.3		
	S_1^*	=	0.33		
	S_2^*	=	1.23		
	ϕ_{cc}	=	0.950		
Factored limit state stress	ϕF_L	=	21.83	MPa	
<i>2. Sections not subject to torsional or torsional-flexural buckling</i>					
					... 3.4.8.2
Largest slenderness ratio for flexural buckling	kL/r	=	173.39		
3.4.10 Uniform compression in components of columns, gross section - flat plates					
<i>1. Uniform compression in components of columns, gross section - flat plates with both edges supported</i>					
					... 3.4.10.1
	k_1	=	0.35		T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	10.5		
	t	=	1	mm	
Slenderness	b/t	=	10.5		



Civil & Structural Engineering Design Services Pty. Ltd.

Limit 1	S_1	=	12.34		
Limit 2	S_2	=	32.87		
Factored limit state stress	ϕF_L	=	228.95	MPa	
Most adverse compressive limit state stress	F_a	=	21.83	MPa	
Most adverse tensile limit state stress	F_a	=	222.70	MPa	
Most adverse compressive & Tensile capacity factor	f_a/F_a	=	0.20		PASS
BENDING - IN-PLANE					
3.4.15 Compression in beams, extreme fibre, gross section rectangular tubes, box sections					
Unbraced length for bending	L_b	=	772	mm	
Second moment of area (weak axis)	I_y	=	1850.2292	mm ⁴	
Torsion modulus	J	=	4291.6056	mm ³	
Elastic section modulus	Z	=	450.39333	mm ³	
Slenderness	S	=	246.78		
Limit 1	S_1	=	0.39		
Limit 2	S_2	=	1695.86		
Factored limit state stress	ϕF_L	=	194.35	MPa	3.4.15(2)
3.4.17 Compression in components of beams (component under uniform compression), gross section - flat plates with both edges supported					
	k_1	=	0.5		T3.3(D)
	k_2	=	2.04		T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	10.5	mm	
	t	=	1	mm	
Slenderness	b/t	=	10.5		
Limit 1	S_1	=	12.34		
Limit 2	S_2	=	46.95		
Factored limit state stress	ϕF_L	=	228.95	MPa	



Civil & Structural Engineering Design Services Pty. Ltd.

Most adverse in-plane bending limit state stress	F_{bx}	=	194.35	MPa		
Most adverse in-plane bending capacity factor	f_{bx}/F_{bx}	=	0.51		PASS	
BENDING - OUT-OF-PLANE						
<i>NOTE: Limit state stresses, ϕF_L are the same for out-of-plane bending (doubly symmetric section)</i>						
Factored limit state stress	ϕF_L	=	194.35	MPa		
Most adverse out-of-plane bending limit state stress	F_{by}	=	194.35	MPa		
Most adverse out-of-plane bending capacity factor	f_{by}/F_{by}	=	0.00		PASS	
COMBINED ACTIONS						
4.1.1 Combined compression and bending						
						...
						4.1.1(2)
	F_a	=	21.83	MPa		... 3.4.8
	F_{ao}	=	228.95	MPa		... 3.4.10
	F_{bx}	=	194.35	MPa		... 3.4.17
	F_{by}	=	194.35	MPa		... 3.4.17
	f_a/F_a	=	0.195			
Check:	$f_a/F_a + f_{bx}/F_{bx} + f_{by}/F_{by}$	\leq	1.0			... 4.1.1 (3)
i.e.	0.70	\leq	1.0		PASS	
SHEAR						
3.4.24 Shear in webs (Major Axis)						
						...
						4.1.1(2)
Clear web height	h	=	23	mm		
	t	=	1	mm		
Slenderness	h/t	=	23			
Limit 1	S_1	=	29.01			
Limit 2	S_2	=	59.31			
Factored limit state stress	ϕF_L	=	131.10	MPa		
Stress From Shear force	f_{sx}	=	V/A_w			
			0.95	MPa		
3.4.25 Shear in webs (Minor Axis)						



Civil & Structural Engineering Design Services Pty. Ltd.

Clear web height	b	=	10.5	mm		
	t	=	1	mm		
Slenderness	b/t	=	10.5			
Factored limit state stress	ϕF_L	=	131.10	MPa		
Stress From Shear force	f_{sy}	=	V/A _w			
			0.00	MPa		

7.2 Legs

NAME	SYMBOL	VALUE	UNIT	NOTES	REF	
HEX45	Legs					
Alloy and temper	6005-T5				AS1664.1	
Tension	F_{tu}	=	262	MPa	<i>Ultimate</i>	T3.3(A)
	F_{ty}	=	241	MPa	<i>Yield</i>	
Compression	F_{cy}	=	241	MPa		
Shear	F_{su}	=	165	MPa	<i>Ultimate</i>	
	F_{sy}	=	138	MPa	<i>Yield</i>	
Bearing	F_{bu}	=	138	MPa	<i>Ultimate</i>	
	F_{by}	=	386	MPa	<i>Yield</i>	
Modulus of elasticity	E	=	70000	MPa	<i>Compressive</i>	
	k_t	=	1			T3.4(B)
	k_c	=	1			
FEM ANALYSIS RESULTS						
Axial force	P	=	0.318	kN	<i>compression</i>	
	P	=	0	kN	<i>Tension</i>	
In plane moment	M_x	=	0.1928	kNm		
Out of plane moment	M_y	=	5.931E-14	kNm		
DESIGN STRESSES						
Gross cross section area	A_g	=	194.7	mm ²		
In-plane elastic section modulus	Z_x	=	2458	mm ³		
Out-of-plane elastic section mod.	Z_y	=	2458	mm ³		
Stress from axial force	f_a	=	P/A _g			
		=	1.63	MPa	<i>compression</i>	



Civil & Structural Engineering Design Services Pty. Ltd.

Stress from in-plane bending	f_{bx}	=	0.00	MPa	Tension	
		=	M_x/Z_x			
		=	78.44	MPa	compression	
Stress from out-of-plane bending	f_{by}	=	M_y/Z_y			
		=	0.00	MPa	compression	
<i>Tension</i>						
3.4.3 Tension in rectangular tubes						
	ϕF_L	=	228.95	MPa		
		OR				
	ϕF_L	=	222.70	MPa		
COMPRESSION						
3.4.8 Compression in columns, axial, gross section						
<i>1. General</i>						
						... 3.4.8.1
Unsupported length of member	L	=	2370	mm		
Effective length factor	k	=	1.00			
Radius of gyration about buckling axis (Y)	r_y	=	14.00	mm		
Radius of gyration about buckling axis (X)	r_x	=	14.00	mm		
Slenderness ratio	kLb/r_y	=	142.86			
Slenderness ratio	kL/r_x	=	169.29			
Slenderness parameter	λ	=	3.162			
	D_c^*	=	90.3			
	S_1^*	=	0.33			
	S_2^*	=	1.23			
	ϕ_{cc}	=	0.950			
Factored limit state stress	ϕF_L	=	22.90	MPa		
<i>2. Sections not subject to torsional or torsional-flexural buckling</i>						
						... 3.4.8.2
Largest slenderness ratio for flexural buckling	kL/r	=	169.29			
3.4.10 Uniform compression in components of columns, gross section - flat plates						
<i>1. Uniform compression in components of columns, gross section - flat plates with both edges supported</i>						
						...
						3.4.10.1
						T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	42			
	t	=	1.5	mm		



Civil & Structural Engineering Design Services Pty. Ltd.

Slenderness	b/t	=	28		
Limit 1	S ₁	=	12.34		
Limit 2	S ₂	=	32.87		
Factored limit state stress	ϕF_L	=	185.00	MPa	
Most adverse compressive limit state stress	F _a	=	22.90	MPa	
Most adverse tensile limit state stress	F _a	=	222.70	MPa	
Most adverse compressive & Tensile capacity factor	f _a /F _a	=	0.07		PASS
BENDING - IN-PLANE					
3.4.15 Compression in beams, extreme fibre, gross section rectangular tubes, box sections					
Unbraced length for bending	L _b	=	2000	mm	
Second moment of area (weak axis)	I _y	=	3.80E+04	mm ⁴	
Torsion modulus	J	=	6.92E+04	mm ³	
Elastic section modulus	Z	=	2458	mm ³	
Slenderness	S	=	191.59		
Limit 1	S ₁	=	0.39		
Limit 2	S ₂	=	1695.86		
Factored limit state stress	ϕF_L	=	198.64	MPa	3.4.15(2)
3.4.17 Compression in components of beams (component under uniform compression), gross section - flat plates with both edges supported					
	k ₁	=	0.5		T3.3(D)
	k ₂	=	2.04		T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	42	mm	
	t	=	1.5	mm	
Slenderness	b/t	=	28		
Limit 1	S ₁	=	12.34		
Limit 2	S ₂	=	46.95		
Factored limit state stress	ϕF_L	=	185.00	MPa	
Most adverse in-plane bending limit state stress	F _{bx}	=	185.00	MPa	



Civil & Structural Engineering Design Services Pty. Ltd.

Most adverse in-plane bending capacity factor	f_{bx}/F_{bx}	=	0.42		PASS	
BENDING - OUT-OF-PLANE						
<i>NOTE: Limit state stresses, ϕF_L are the same for out-of-plane bending (doubly symmetric section)</i>						
Factored limit state stress	ϕF_L	=	185.00	MPa		
Most adverse out-of-plane bending limit state stress	F_{by}	=	185.00	MPa		
Most adverse out-of-plane bending capacity factor	f_{by}/F_{by}	=	0.00		PASS	
COMBINED ACTIONS						
4.1.1 Combined compression and bending						
	F_a	=	22.90	MPa		... 4.1.1(2)
	F_{ao}	=	185.00	MPa		... 3.4.8
	F_{bx}	=	185.00	MPa		... 3.4.10
	F_{by}	=	185.00	MPa		... 3.4.17
	f_a/F_a	=	0.071			... 3.4.17
	Check: $f_a/F_a + f_{bx}/F_{bx} + f_{by}/F_{by} \leq 1.0$... 4.1.1 (3)
	i.e. $0.50 \leq 1.0$				PASS	
SHEAR						
3.4.24 Shear in webs (Major Axis)						
						... 4.1.1(2)
Clear web height	h	=	42	mm		
	t	=	1.5	mm		
Slenderness	h/t	=	28			
Limit 1	S_1	=	29.01			
Limit 2	S_2	=	59.31			
Factored limit state stress	ϕF_L	=	131.10	MPa		
Stress From Shear force	f_{sx}	=	V/A_w			
			0.59	MPa		
3.4.25 Shear in webs (Minor Axis)						
Clear web height	b	=	42	mm		
	t	=	1.5	mm		



Civil & Structural Engineering Design Services Pty. Ltd.

Slenderness	b/t	=	28		
Factored limit state stress	ϕF_L	=	131.10	MPa	
Stress From Shear force	f_{sy}	=	V/A_w		
			0.00	MPa	

7.3 Centre Pole

NAME	SYMBOL	VALUE	UNIT	NOTES	REF
HEX45	Centre Pole				
Alloy and temper	6005-T5				AS1664.1
Tension	F_{tu}	=	262	MPa	<i>Ultimate</i>
	F_{ty}	=	241	MPa	<i>Yield</i>
Compression	F_{cy}	=	241	MPa	
Shear	F_{su}	=	165	MPa	<i>Ultimate</i>
	F_{sy}	=	138	MPa	<i>Yield</i>
Bearing	F_{bu}	=	138	MPa	<i>Ultimate</i>
	F_{by}	=	386	MPa	<i>Yield</i>
Modulus of elasticity	E	=	70000	MPa	<i>Compressive</i>
	k_t	=	1		
	k_c	=	1		
FEM ANALYSIS RESULTS					
Axial force	P	=	0.096	kN	<i>compression</i>
	P	=	0	kN	<i>Tension</i>
In plane moment	M_x	=	0.0508	kNm	
Out of plane moment	M_y	=	1.644E-16	kNm	
DESIGN STRESSES					
Gross cross section area	A_g	=	194.7	mm ²	
In-plane elastic section modulus	Z_x	=	2458	mm ³	
Out-of-plane elastic section mod.	Z_y	=	2458	mm ³	
Stress from axial force	f_a	=	P/A_g		
		=	0.49	MPa	<i>compression</i>
		=	0.00	MPa	<i>Tension</i>
Stress from in-plane bending	f_{bx}	=	M_x/Z_x		



Civil & Structural Engineering Design Services Pty. Ltd.

		=	20.67	MPa	<i>compression</i>	
Stress from out-of-plane bending	f_{by}	=	M_y/Z_y			
		=	0.00	MPa	<i>compression</i>	
<i>Tension</i>						
3.4.3 Tension in rectangular tubes						
	ϕF_L	=	228.95	MPa		
		OR				
	ϕF_L	=	222.70	MPa		
COMPRESSION						
3.4.8 Compression in columns, axial, gross section						
<i>1. General</i>						
						... 3.4.8.1
Unsupported length of member	L	=	1290	mm		
Effective length factor	k	=	1.00			
Radius of gyration about buckling axis (Y)	r_y	=	14.00	mm		
Radius of gyration about buckling axis (X)	r_x	=	14.00	mm		
Slenderness ratio	kLb/r_y	=	65.71			
Slenderness ratio	kL/r_x	=	92.14			
Slenderness parameter	λ	=	1.72			
	D_c^*	=	90.3			
	S_1^*	=	0.33			
	S_2^*	=	1.23			
	ϕ_{cc}	=	0.821			
Factored limit state stress	ϕF_L	=	66.80	MPa		
<i>2. Sections not subject to torsional or torsional-flexural buckling</i>						
						... 3.4.8.2
Largest slenderness ratio for flexural buckling	kL/r	=	92.14			
3.4.10 Uniform compression in components of columns, gross section - flat plates						
<i>1. Uniform compression in components of columns, gross section - flat plates with both edges supported</i>						
						... 3.4.10.1 T3.3(D)
	k_1	=	0.35			
Max. distance between toes of fillets of supporting elements for plate	b'	=	42			
	t	=	1.5	mm		
Slenderness	b/t	=	28			



Civil & Structural Engineering Design Services Pty. Ltd.

Limit 1	S_1	=	12.34		
Limit 2	S_2	=	32.87		
Factored limit state stress	ϕF_L	=	185.00	MPa	
Most adverse compressive limit state stress	F_a	=	66.80	MPa	
Most adverse tensile limit state stress	F_a	=	222.70	MPa	
Most adverse compressive & Tensile capacity factor	f_a/F_a	=	0.01		PASS
BENDING - IN-PLANE					
3.4.15 <i>Compression in beams, extreme fibre, gross section rectangular tubes, box sections</i>					
Unbraced length for bending	L_b	=	920	mm	
Second moment of area (weak axis)	I_y	=	3.80E+04	mm ⁴	
Torsion modulus	J	=	6.92E+04	mm ³	
Elastic section modulus	Z	=	2458	mm ³	
Slenderness	S	=	88.13		
Limit 1	S_1	=	0.39		
Limit 2	S_2	=	1695.86		
Factored limit state stress	ϕF_L	=	208.85	MPa	3.4.15(2)
3.4.17 <i>Compression in components of beams (component under uniform compression), gross section - flat plates with both edges supported</i>					
	k_1	=	0.5		T3.3(D)
	k_2	=	2.04		T3.3(D)
Max. distance between toes of fillets of supporting elements for plate	b'	=	42	mm	
	t	=	1.5	mm	
Slenderness	b/t	=	28		
Limit 1	S_1	=	12.34		
Limit 2	S_2	=	46.95		
Factored limit state stress	ϕF_L	=	185.00	MPa	
Most adverse in-plane bending limit state stress	F_{bx}	=	185.00	MPa	



Civil & Structural Engineering Design Services Pty. Ltd.

Most adverse in-plane bending capacity factor	f_{bx}/F_{bx}	=	0.11		PASS	
BENDING - OUT-OF-PLANE						
<i>NOTE: Limit state stresses, ϕF_L are the same for out-of-plane bending (doubly symmetric section)</i>						
Factored limit state stress	ϕF_L	=	185.00	MPa		
Most adverse out-of-plane bending limit state stress	F_{by}	=	185.00	MPa		
Most adverse out-of-plane bending capacity factor	f_{by}/F_{by}	=	0.00		PASS	
COMBINED ACTIONS						
4.1.1 Combined compression and bending						
						...
						4.1.1(2)
	F_a	=	66.80	MPa		... 3.4.8
	F_{ao}	=	185.00	MPa		... 3.4.10
	F_{bx}	=	185.00	MPa		... 3.4.17
	F_{by}	=	185.00	MPa		... 3.4.17
	f_a/F_a	=	0.007			
	Check: $f_a/F_a + f_{bx}/F_{bx} + f_{by}/F_{by} \leq 1.0$... 4.1.1 (3)
	i.e. $0.12 \leq 1.0$				PASS	
SHEAR						
3.4.24 Shear in webs (Major Axis)						
						...
						4.1.1(2)
Clear web height	h	=	42	mm		
	t	=	1.5	mm		
Slenderness	h/t	=	28			
Limit 1	S_1	=	29.01			
Limit 2	S_2	=	59.31			
Factored limit state stress	ϕF_L	=	131.10	MPa		
Stress From Shear force	f_{sx}	=	V/A_w			
			0.34	MPa		
3.4.25 Shear in webs (Minor Axis)						
Clear web height	b	=	42	mm		
	t	=	1.5	mm		



Civil & Structural Engineering Design Services Pty. Ltd.

Slenderness	b/t	=	28			
Factored limit state stress	ϕF_L	=	131.10	MPa		
Stress From Shear force	f_{sy}	=	V/A_w			
			0.00	MPa		



Civil & Structural Engineering Design Services Pty. Ltd.

8 Summary

8.1 Conclusions

- a. The $3\text{m} \times 3\text{m}$, $3\text{m} \times 4.5\text{m}$ & $3\text{m} \times 6\text{m}$ HEX 45A Folding Marquees as specified have been analyzed with a conclusion that they have the capacity to withstand wind speeds up to and including **50km/hr**.
- b. For forecast winds in excess of **50km/hr** – the structure should be completely folded.
- c. For uplift due to 50km/hr, 0.4 kN (40kg) holding down weight/per leg for middle legs and 20kg for corner legs are required.
- d. No Fabrics or doors should be used for covering the sides of unbraced Folding Marquees due to the lack of bracing within the system and insufficient out-of-plane stiffness of framing.

Yours faithfully,

E.A. Bennett M.I.E. Aust. NPER 198230



Civil & Structural Engineering Design Services Pty. Ltd.



C & SITE-IT

Civil & Structural Engineering Design Services Pty. Ltd.

ABN: 62 051 307 852

3 Wanniti Road BELROSE NSW 2085

Email: hited@bigpond.net.au

Tel: 02 9975 3899 Fax: 02 99751943

Web: www.civilandstructural.com.au

05th April 2021

Hercules Instant Shelter Australias
17/256 Musgrave Road
Coopers Plains QLD 4108

Dear Sir/Madam,

Certificate of Adequacy for Design of Temporary Structures Folding Marquee – HEX 45A

I, Edward A. Bennett, practicing structural Engineer, hereby certify that I have carried out computations in accordance with proper design principles for the purpose of certifying the structural adequacy of the above marquees to be erected as a temporary structure at various Sites throughout Australia that meet the Design Restrictions and Limitations within the computations (Copy of Report attached).

I am able to confirm that these Temporary Structures will be erected with weights/tie downs in accordance with the BCA Section B, “Structural Provisions”, AS 1170.0 & 1-2002, “Structural Design Actions” and AS 1170.2, 2011 “Wind Actions”, such that I am able to issue this “Certificate of Adequacy - Design”.

Full Name of Designer:	Edward Arthur Bennett
Qualifications:	M.I.E. Aust. CPE NPER 198230
Address of Designer:	3 Wanniti Road, Belrose NSW 2085
Business Telephone No.:	Phone: (02) 9975 3899 Fax: 9974 1943
Name of Employer:	Civil & Structural Engineering Design Services Pty. Ltd.

Yours faithfully,

E.A. Bennett M.I.E. Aust. NPER 198230, BPB NSW-0282, BPB VIC – EC 25923 & RPEQ 4541



HEX 45A ROBUST & LIGHT WEIGHT ALLOY

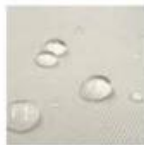
Hex 45A features ultra light 45mm profile aluminium hexagonal legs. This frame has been developed into an unique balance between light weight and strength. It is also the lightest folding marquee in our range.

Main Features

- 1 Minute set up. No loose parts, no tools are required!
- 45mm Hexagonal, 1.5mm Thickness alloy outer legs.
- 25 x 12.5mm Cross bracing truss bars.
- All legs and truss bars are made from an unique ultra light weight aluminium yet strong.
- All joints are made from reinforced nylon.
- Quick lock release pull-pins for finger protection.



Specification



Waterproof & UV Treated Fabric, standard package comes with the thick 500D PVC coated polyester fabric.



All Seam Points Are Double Stitched for added strength and durability.



Sturdy Center Pole ensures proper top up-right.



Central Pivot Design ensures lifetime of durability.



Supported Buckled Strap. The canopy is secured to the frame with additional buckled strap at 4-sides.



Protective Layer At Corners, a double lining reinforcement for extra protection.



Reinforced Nylon Brackets are joined to structural components with anti-rust bolts, offer durable and robust result.



Pull-pin Quick Lock Release Button with 2 height levels adjustment reaching maximum of 2.1 meter.



Stainless Steel Thick Footplates with holes provided for pegs.



50mm Wide Velcro Strap. Sidewalls can be easier attached on the canopy.

WON'T BE BEATON ON PRICE & QUALITY + NATIONWIDE DELIVERY

Warranty



The HEX45 A Marquee is covered by 3 years framework warranty.

Sizes

2.5m x 2.5m – 15kg
3m x 3m – 16kg
3m x 4.5m – 21kg
3m x 6m – 30kg

Colors

9 Standard colors available:

 Black, White, Grey, Red, Blue, Green, Navy, Maroon, Yellow.

Accessories

Solid full wall/door wall
Half wall/Window wall
PVC clear wall/Mesh wall
Sandbag/Steel leg weight
Carry bag/Wheelie bag
Rain Gutter

Phone: 1300 810 910 | Email: sales@herculesinstantshelter.com.au | www.herculesinstantshelter.com.au